



Quality	X3CrNiCu18-9-4				Austenitic Stainless Steel			<i>Technical card 2018</i>
Number	1.4567				Lucefin Group			

Chemical composition

C%	Si%	Mn%	P%	S% a)	Cr%	Ni%	N%	Cu% b)
max	max	max	max	max			max	
0,04	1,00	2,00	0,045	0,030	17,0-19,0	8,5-10,5	0,10	3,0-4,0
± 0,01	+ 0,05	± 0,04	+ 0,005	± 0,005	± 0,2	± 0,1	+ 0,01	± 0,1

Product deviations are allowed

a) for improving machinability, it is suggested a controlled sulphur content of 0,015 % - 0,030 %

b) for steel intended to cold-work hardening and extrusion, it is allowed a Cu content of max 1,0 %

a) for polishability, it is suggested a controlled sulphur content of max 0,015 %

Temperature °C

Melting range	Hot-forming	Solution annealing (Solubilization) +AT	Stabilizing	Soft annealing +A	MMA welding – AWS electrodes pre-heating	post welding	
1450-1400	1200-900	1100-1000 water	not necessary	not suitable	not necessary	slow cooling	
Sensitization	Quenching +Q	Tempering +T			<i>joint with steel</i>		
sensitization test at 700-450	not suitable	not suitable			carbon	CrMo alloyed	stainless
					E 316L	E 316L	E 316L
					<i>cosmetic welding</i>		
					E 316L		

Chemical treatment • Pickling (6 - 25% HNO₃) + (0,5 - 8% HF) hot or cold. **Passivation** 20 - 45% HNO₃ cold**Mechanical properties**

Heat-treated material EN 10088-3: 2014 in conditions 1C, 1E, 1D, 1X, 1G, 2D

size	Testing at room temperature							
mm	R	R _p 0,2	A%	A%	Kv ₂ +20 °C	Kv ₂ +20 °C	HBW ^{a)}	
from to	N/mm ²	N/mm ² min	min (L)	min (T)	J min (L)	J min (T)	max	
160	450-650	175	45	-	-	-	215	+AT solubilization

a) for information only

(L) = longitudinal (T) = transversal

Bright bars of heat-treated material EN 10088-3: 2014 in conditions 2H, 2B, 2G, 2P

size	Testing at room temperature							
mm	R	R _p 0,2	A%	A%	Kv ₂ +20 °C	Kv ₂ +20 °C		
from to	N/mm ²	N/mm ² min	min (L)	min (T)	J min (L)	J min (T)		
10 ^{b)}	600-850	400	25	-	-	-		
10	600-850	340	25	-	-	-		+AT solubilization
16	450-800	175	30	-	100	-		
40	63	450-800	175	30	-	100	-	
63	160	450-650	175	40	-	100	-	

b) in the range of 1 mm ≤ d < 5 mm, values are valid only for rounds – the mechanical properties of non round bars of < 5 mm of thickness have to be agreed at the time of request and order

(L) = longitudinal (T) = transversal

Forged

size	Testing at room temperature							
mm	R	R _p 0,2	A%	A%	Kv +20 °C	HB ^{a)}		
from to	N/mm ²	N/mm ² min	min (L)	min (T)	J min (L)	max		
-	-	-	-	-	-	215		+AT solubilization

a) for information only

Effect of cold-working (hot-rolled +AT+C). Approximate values

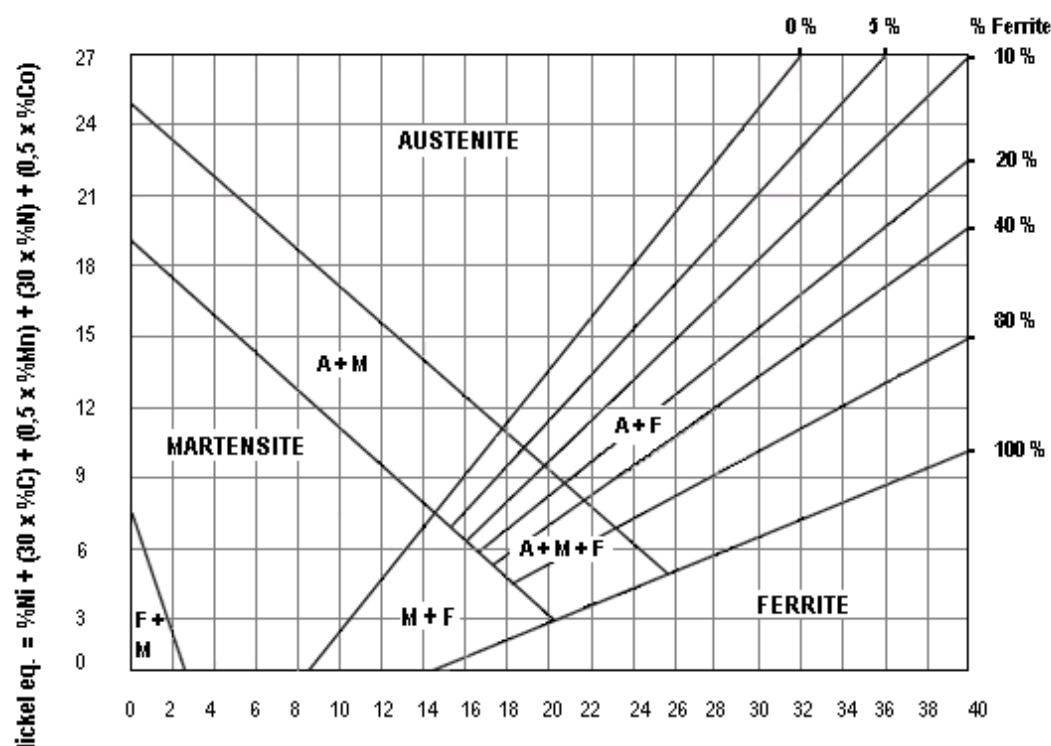
R	N/mm ²	560	720	820	940	1010	1120	1180	1300	1380
R _p 0,2	N/mm ²	300	560	710	820	900	990	1070	1200	1270
A	%	60	30	18	12	10	8	8	8	8
Reduction %		0	10	20	30	40	50	60	70	75

Thermal expansion	$10^{-6} \cdot K^{-1}$	►	16.7	17.2	17.7	18.1	
Modulus of elasticity	longitudinal GPa	200	194	186	179	172	127
Poisson number	ν	0.28					
Electrical resistivity	$\Omega \cdot mm^2/m$	0.73					
Electrical conductivity	Siemens.m/mm ²	1.33					
Specific heat	J/(Kg.K)	500					
Density	Kg/dm ³	7.90					
Thermal conductivity	W/(m.K)	15.0	16.6				
Relative magnetic permeability	μ_r max	1.02					
°C	20	100	200	300	400	600	800

The symbol ► indicates temperature between 20 °C and 100 °C, 20 °C and 200 °C

Corrosion resistance		Atmospheric		Chemical			x intercrystalline c. pitting, urban water, stress corrosion
Fresh water		industrial marine		medium oxidizing		reducing	
x		x		x	x		
Magnetic	no						
Machinability	high						
Hardening	cold-drawn and other cold plastic deformations						
Service temperature in air	continuous service up to 850 °C; intermittent service up to 800 °C						
Europe EN	USA UNS	USA ASTM	China GB	Russia GOST	Japan JIS	India IS	Republic of Korea KS
X3CrNiCu18-9-4	S30430		06Cr18Ni9Cu3		SUS XM7		STS XM7

Schaeffler diagram (extended formulas)



$$\text{Chromium eq.} = \%Cr + \%Mo + (0.5 \times (\%Nb + \%Ta)) + (1.5 \times \%Si) + (2 \times \%Ti) + (\%W + \%V + \%Al)$$

The diagram is divided into three main areas which correspond to the structures of the weld bead: austenitic, ferritic and martensitic. Thanks to this calculation method, it is possible to determine before-hand the structures which are likely to be present in the weld bead and therefore to correctly choose the weld material according to the desired final structure.